



Sun S.B. Co. № 39.

General Arrangement  
S.S. "J.N. Pew"

Report № 4213

XII81-0101



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## ALTERATIONS

## MATERIAL

## PRINCIPAL DIMENSIONS

LENGTH B.P.	480'-0"
BEAM (MOLDED.)	65'-9"
DEPTH (MOLDED TO SHELTER DECK)	37'-0"

**CHARGE**

ACTION

SCALE - ARRANG'T =  $\frac{1}{16}$ " = 1 FT.  
SCALE - DETAIL =  $\frac{1}{16}$ " = 1 FT. DATE 11-20-20

DEL'N	TRACED	CHECKED	APPROVED
ALT.	ALT.	XG.	<i>John C. Shidell</i>

# SUN SHIPBUILDING CO.

Sun S.B.C. N° 39.

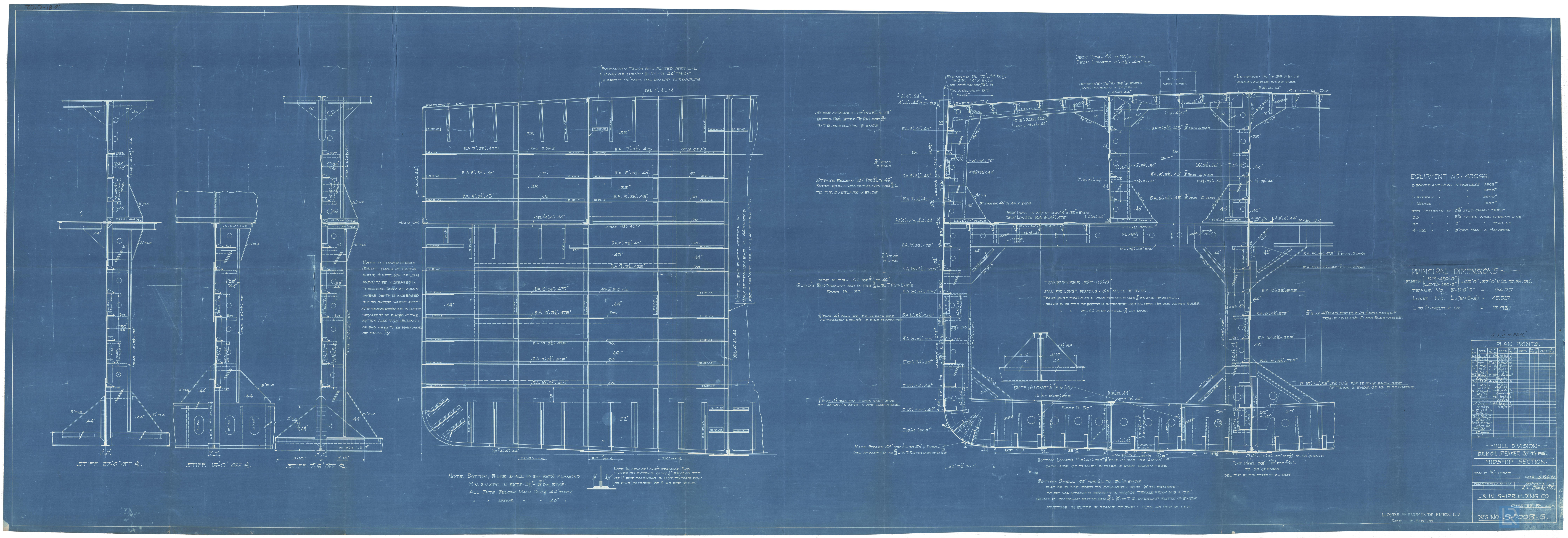
Midship Section  
S.S. "J. N. Pew"

Report N° 42/3.

W181-0102



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NOTE

ALL CAULKING EDGES OF BOILER PLATE TO BE MACHINE PLANED.

SEAMS BUTTS AND LAPS TO FIT CLOSELY, DRAWN UP METAL TO METAL AND AFTER BEING RIVETED.

CAULKED INSIDE AND OUTSIDE.

ALL REINFORCE PLATES TO BE CAULKED.

CONSTRUCTED UNDER THE BOARD OF SUPERVISING  
INSPECTORS DEPT OF COMMERCE & LLOYDS RULES  
FOR 200LBS WORKING PRESSURE

DESCRIPTION	THICKNESS	U.S. RULES	LLOYD'S RULES	
SHELL	13/32	$P = \frac{60000 \times 1.59375}{6 \times 95} + 20\% = 201$ #	$P = \frac{2104 \times (25.5-2) \times 84.2}{191.59375} = 217$ #	BOILER DATA
FURNACE	21/32	$P = \frac{15600 \times .65625}{50} = 204$ #	$P = \frac{1259 \times (10.5-2)}{52.3125} = 204$ #	TUBES
TOP HEAD PLATE	1/8	$P = \frac{175 \times 18^2}{270} = 210$ #	$P = \frac{175 \times 18^2}{270} = 210$ #	FURNACES
TOP HEAD STAY	21/16	$S = \frac{16.875 \times 16 \times 200}{6.2126} = 86.92$ #	$P = \frac{10400 \times 6.2126}{16.875 \times 16} = 239$ #	COMB. CHAMB
TUBE PLATE	3/4	$P = \frac{(3.75-2.23) \times 75 \times 27000}{40 \times 3.75} = 205$ #	$P = \frac{3.75-2.23 \times 1750 \times 12}{40 \times 3.75} = 212.8$ #	BACK TUBE PLATE
C.C. CROWN PLATE	21/32	$P = \frac{135 \times 10.5^2}{71.19} = 209$ #	$P = \frac{135 \times 10.5^2}{71.19} = 209$ #	TOTAL H.S.
C.C. CROWN STAYS	1/4	$S = \frac{8.375 \times 8.5 \times 200}{1.997} = 712.9$ #	$P = \frac{7500 \times 1.997}{8.375 \times 8.5} = 210$ #	GRATE SUR.
WRAPPER PLATE	21/32	$P = \frac{120 \times 10.5^2}{54.125} = 244$ #	$P = \frac{100 \times 10.5^2}{54.125} = 203$ #	H.S./G.S.
WRAPPER STAYS	1/4	$S = \frac{8.5 \times 6 \times 200}{1.997} = 510.7$ #	$P = \frac{7500 \times 1.997}{8.5 \times 6} = 293$ #	CALORIMETER
C.C. BACK PLATE	3/4	$P = \frac{120 \times 12^2}{68.125} = 253$ #	$P = \frac{100 \times 12^2}{68.125} = 211$ #	G.S./CAL
C.C. BACK STAYS	1 3/4	$S = \frac{8.5 \times 8 \times 200}{1.997} = 680.5$ #	$P = \frac{7500 \times 1.997}{8 \times 8.5} = 220$ #	LENGTH OF GRATE
CROWN GIRDERS	10 1/2 x 1	$\frac{917 \times 10.5^2 \times 2}{(41.5-8.5) \times 8.375 \times 3.45} = 212$ #	$P = \frac{11850 \times 10.5^2 \times 2}{(40-8.5) \times 8.375 \times 40} = 247$ #	
BOTTOM COMB. CH.	1"	$S = \frac{50[(300 \times 1) - (2 \times 36.5)]}{54.5} = 208$ #	$P = \frac{50(300 \times 1 - 40)}{54.5} = 238$ #	
WIDE WATER SPACE FRONT	1"		$P = \frac{140 \times 16^2}{132} = 212$ #	

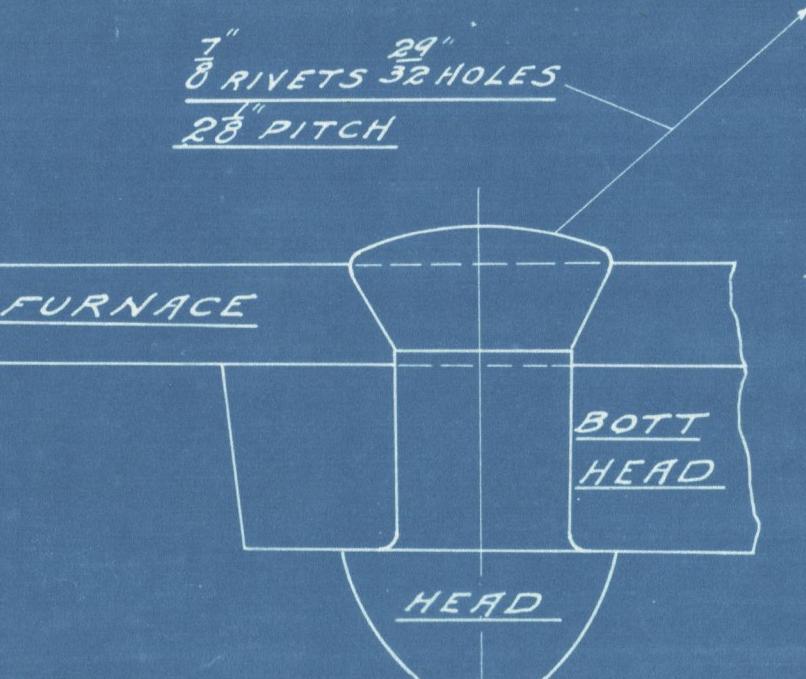
TENSILE STRENGTH OF SHELL PLATES 60,000 TO 70,000 LBS  
" " " FLANGE " 55,000 TO 65,000 LBS.  
" " " GIRDERS 60,000 TO 70,000 LBS  
WORKING PRESSURE 200# PER SQ IN

WATER TEST 300\* " " "

EVAPORATION 270 LBS OF WATER PER SQ. FOOT  
OF GRATE PER HOUR.

3 $\frac{1}{2}$  TWIN SAFETY VALVE COMBINED AREA 19.24

FOR DETAIL OF BOTTOM HEAD  
STEAM EJECTOR NO. 8123



**SUN SHIPBUILDING COMPANY**  
**CHESTER, PENNA., U.S.A.**  
**ENGINEERING DEPARTMENT.**

15<sup>FT</sup> 10" INS. DIA. x 11<sup>FT</sup> 11<sup>1/4</sup>" BETW. HEADS.  
S.E. SCOTCH BOILER  
200 LBS. WORKING PRESSURE

DRAWN BY J.B. CHIEF DRAFTSMAN E. J. Pauliffe  
TRACED BY J.B.  
CHECKED BY K.P.R. APPROVED A.A. Howell  
DATE 26 Feb 20  
SCALE 11 1" = 1 FT. CHIEF ENGINEER

DR. 39-862-1

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
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and W. H. Penn

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Sew S. B.  
Arrgt of Shaffing

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7/<sub>8</sub>" TOTAL LENGTH.

6 ET 4" LENGTH OF TAIL SH

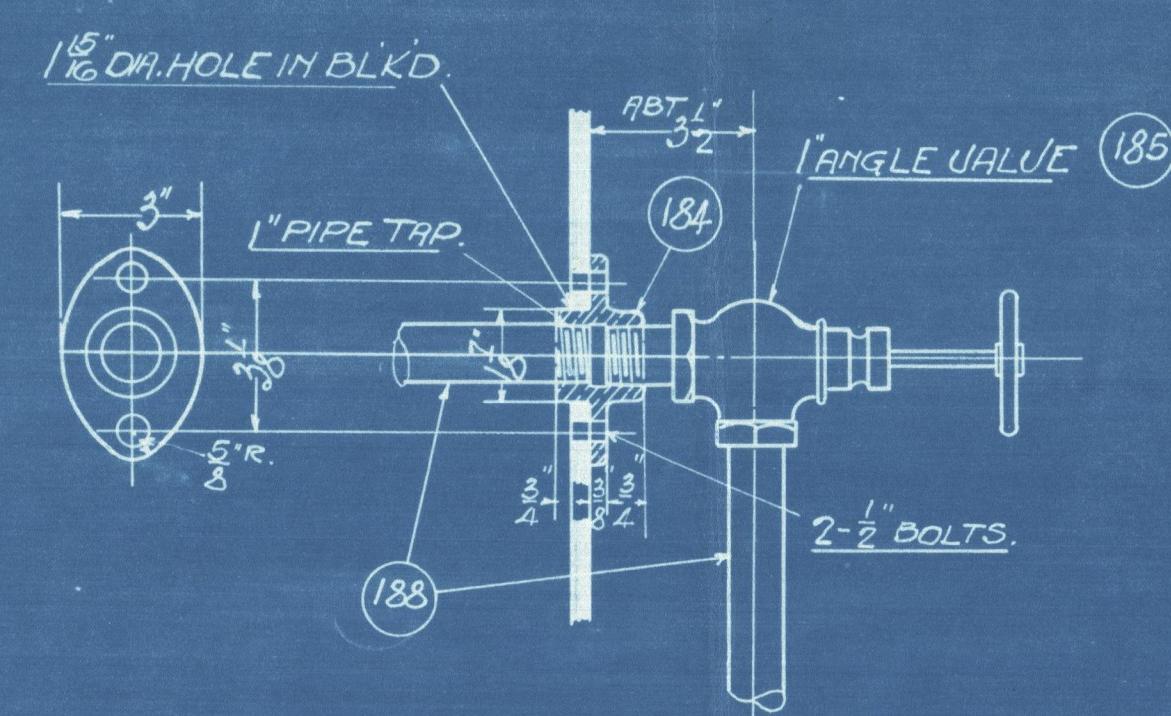
1 FT 11 7/8" LENGTH OF LINE

QFT-O" LENGTH  
THRUST SHAFT

28ET3" LENGTH CRAN

VIEW SHOWING SEQUENCE OF CRANKS  
LOOKING AFT

*DETAIL OF WATER CIRCULATING CONNECTION.*



SIZE OF ENGINE - 27' x 45'  
BOILER PRESSURE - 20  
DIA. OF PROPELLER - 1

S ON SHAFTING BY LLOYD'S RULES FOR SHAFTING  
DIAM. OF INTERMEDIATE SHAFT.

$$t.009 \times 45.5 + .002 \times 76 + .0165 \times 51) \times \sqrt[3]{200} = 14.2 \text{ " DIA. MADE}$$

1. OF CRANK & THRUST SHAFT UNDER COLLARS.

$$\frac{14.2 \times 21}{20} = 14.9 \text{ " DIA. - MADE } 15\frac{1}{4} \text{ " DIA.}$$

DIAM. OF TAIL SHAFT.

$$4.2 \times (.63 + \frac{.03 \times 228}{14.2}) = 15.76 \text{ - MADE } 16\frac{1}{8} \text{ " DIA.}$$

LIST OF DETAIL DRAWINGS	
TITLE	DR. NO.
LINE SHAFT FORGINGS	39-842
TURN TUBE	37-842
DETAILS OF SHAFTING	39-842
THRUST BEARING	1-840-
THRUST BEARING BED PLATE	1-840-
HORSE SHOE BEARING	1-840-
LINE SHAFT BEARING	1-840-8
RANK SHIFT.	39-814-2

## ARRANGEMENT OF SHAFTING.

B/M NUM 39-820			
		DRAWN BY WAM	
		TRACED BY WAM	
		CH'K'D BY <u>Unifffe</u>	
		DATE 2 September 20	APPROVED <u>A.A. Howitt</u>